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2 **Improvement and performance testing of melting system for measurement of trace**  
3 **elements in firn core drilled at NEEM site, Greenland**

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## SUPPLEMENTARY MATERIAL

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### 21 **Operating procedures of the melting system**

22       The operating procedures of the firm core melting system were similar to those reported by Hong and  
23 others (2015) [1] with modifications to the cleaning method of the melting system between melting  
24 procedures to reduce the system BLs of elements.

25       The PFA and PTFE connection tubes and peristaltic pumping tubes were connected to the melting  
26 head and were rinsed with UPW, 1% HNO<sub>3</sub> (ultra grade), and 0.1% HNO<sub>3</sub> (ultra grade) for 10 min each,  
27 and then again with UPW for 20 min. After the melting head had been assembled into the melting system  
28 inside the freezer, the temperature of the heating body was controlled at  $\sim 38 \pm 2^\circ\text{C}$  (type A melting  
29 head) or  $\sim 33 \pm 2^\circ\text{C}$  (type B melting head). Then, the surface temperature of the melting head was  
30 consistently checked, especially when the temperature inside the freezer fell below  $0^\circ\text{C}$ .

31       Before the firm core samples were melted using the melting system, the melting processes were  
32 tested with AIC sections to confirm that the system was properly operating. Key parameters, including the  
33 melting rate and the volumes of the melted samples from the inner and outer zones of the melting head,  
34 were also continuously examined during melting of the firm cores. It is important to periodically exchange  
35 the peristaltic pumping tubes because their elasticity can affect the draining rate of the melted samples

36 through the inner and outer zones. In addition, when the tubes were not in use, they were disconnected to  
37 maintain their flexibility.

38 After the AICs had been melted, the melting system was cleaned with  $\sim 25 \pm 5$  mL UPW ( $\sim 40 \pm$   
39  $5$  mL  $0.1\%$   $\text{HNO}_3$  (ultra grade), and then  $\sim 40 \pm 5$  mL UPW for the type B-head melter) through the  
40 type A melting head, and  $\sim 20$  mL UPW ( $\sim 10$  mL UPW for the type B-head melter) through just the  
41 inner zone of the melting head. Then,  $\sim 10$  mL UPW that had flowed out from the inner zone was  
42 collected as a system blank to examine the cleanliness of the melting system. The firn core section was  
43 placed on the melting head after chiseling the bottom of the core with a clean ceramic knife (FK-110WH,  
44 Japan) in case the temperature inside the freezer again fell below  $0^\circ\text{C}$ . It is crucial that the temperature  
45 inside the freezer should remain below  $0^\circ\text{C}$  during melting procedures to prevent any melting of the firn  
46 core due to the ambient temperature. The melted samples flowed out from the freezer through PFA  
47 connection tubes capped with insulating tubes and were collected discretely in sample collection bottles  
48 with a depth resolution of  $\sim 11 \pm 2$  cm. The depth resolution was determined based on the accumulation  
49 rate of the drilling site and research objectives. The sample collection bottles used for trace elements were  
50 thoroughly cleaned using a well established method [2]. After the firn core samples had been melted, the  
51 system blanks ( $\sim 10$  mL UPW drained through just the inner zone) were also continuously collected to  
52 examine the levels of elements that remained in parts of the melting system.

53 After the melting processes was complete each day, the melting system was cleaned again by  
54 passing  $\sim 40 \pm 5$  mL UPW through the melting head, and the bottom of melting head in direct contact  
55 with the heating body was also thoroughly cleaned with UPW. Then, 0.1% HNO<sub>3</sub> (ultra grade) was  
56 circulated slowly overnight through the melting head attached to the connection tubes (PFA, PTFE, and  
57 peristaltic pumping tubes).

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#### 59 **Cleanliness of laminar flow hood**

60 The concentrations of dust with diameter larger than 0.5- $\mu$ m were consistently measured near the  
61 sample collection bottles and the melting head during the preparation period. The dust concentrations  
62 measured in the air around the melting system indicated suitable cleanliness during firm core melting  
63 procedures. Although the dust concentrations near the sample collection bottles sometimes reached  $\sim 1060$   
64 particles m<sup>-3</sup>, they were generally close to zero, which verifies the clean conditions of the air surrounding  
65 the bottles. Near the melting head, dust concentration levels were  $\sim 10600$ – $14100$  particles m<sup>-3</sup> in the early  
66 stage of the preparation period but mostly less than  $\sim 3500$  particles m<sup>-3</sup>. These results indicate that the  
67 concentrations of dust around the melting head were generally higher than those near the sample  
68 collection bottles. This is primarily due to the dispersed dust from the floor by the opening and closing of  
69 the refrigerator door and also the cooling fan operating in the bottom of the freezer, despite the fact that  
70 an adhesive mat had been placed on the floor in front of the refrigerator.

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73 Table S1. Analytical conditions of inductively coupled plasma sector field mass spectrometry (ICP-  
74 SFMS) for the analysis of trace elements in melted sample of firn cores

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	Description
System	HR ICP-MS (Element 2)
Plasma power	1250 W
Cool gas	16 L min <sup>-1</sup>
Aux gas	0.73 L min <sup>-1</sup>
Sample gas	0.93 L min <sup>-1</sup>
Guard Electrode	Yes
Sample introduction	Apex with Actively Cooled Membrane (ACM)
Instrumental sensitivity	daily optimized (~1000000 cps for <sup>115</sup> In/ ~1500000 cps for <sup>238</sup> U)
Double charged ion level	<9 % ( <sup>137</sup> Ba <sup>2+</sup> / <sup>137</sup> Ba)
Oxide level	<0.1 % ( <sup>137</sup> BaO/ <sup>137</sup> Ba)
Stability	<1 %

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78 Table S2. Instrumental detection limits and accuracy tests of inductively coupled plasma sector field mass  
 79 spectrometry (unit: ng L<sup>-1</sup>)

Element	IDL <sup>a</sup>	Measured conc.	Certified conc. <sup>b</sup>	RE(%) <sup>c</sup>
V(MR)	0.087	404.2	317±33	-27.5
Cr(MR)	0.824	239.9	208±23	-15.4
Mn(MR)	0.250	4433.4	4330±180	-2.4
Co(MR)	0.075	57.4	50 <sup>d</sup>	-14.8
Rb(LR)	0.030	1282.7	1240±370 <sup>e</sup>	-3.4
Sr(LR)	0.114	57591.1	53600±1300	-7.4
Cd(LR)	0.028	7.7	6±1.4	-28.1
Ba(LR)	0.127	15602.0	14000±500	-11.4
Tl(LR)	0.021	4.3	3.9±2.4 <sup>e</sup>	-11.1
Pb(LR)	0.064	75.7	81±6	6.6
Th(LR)	0.129	15.0	13.6±3.3 <sup>e</sup>	-10.0
U(LR)	0.018	92.3	93±6	0.8

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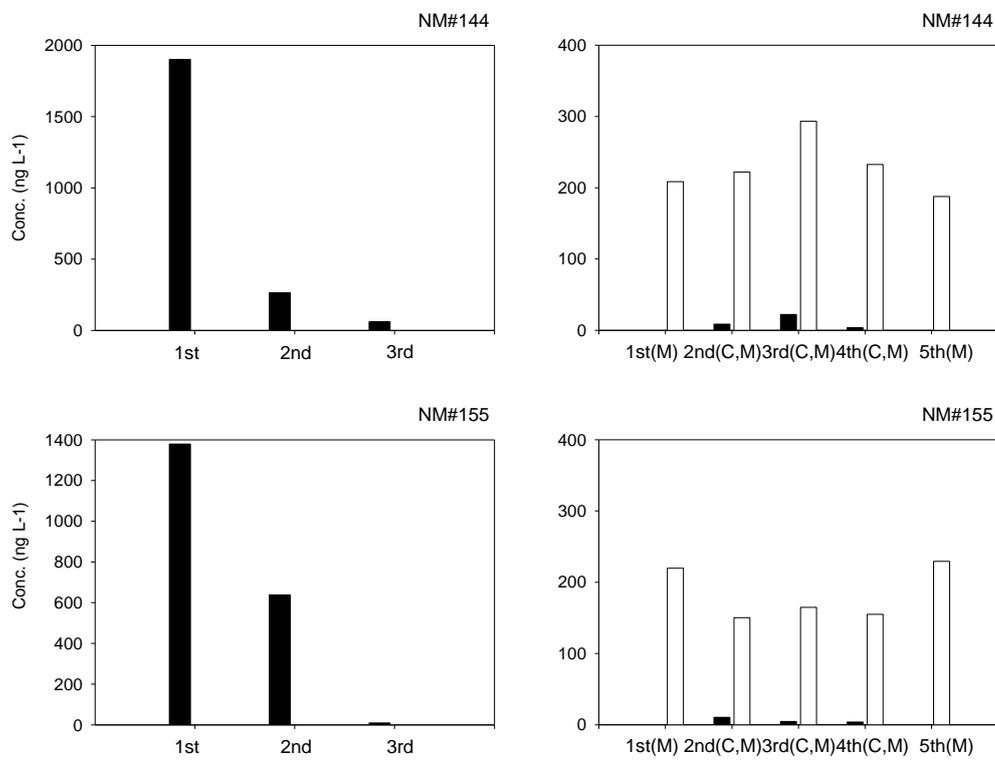
81 <sup>a</sup> Instrumental detection limit (IDL) was calculated by 3σ of 12 distilled water samples

82 <sup>b</sup> Certified values of CRM (SLRS5) [3], <sup>c</sup> Relative error, <sup>d</sup> Information values [3], <sup>e</sup> Reference values [4]

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87 Figure S1. Comparison of concentrations of Cu in firn core samples (NEEM #144, NEEM #155) from  
88 conventional chiseling and melting method with FEP coated Cu melting head (black bar: chiseling  
89 technique, white bar: melting method, 1st, 2nd, and 3rd layers indicates sliced samples in series from the  
90 outer most surface and 2nd(C,M), 3rd(C,M), and 4th(C,M) indicates 2nd, 3rd, and 4th decontaminated  
91 samples with depth resolution of ~10cm in the inner part using chiseling and melting method,  
92 respectively)

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